

# Development of a TLP substructure for a 6MW wind turbine based on development of a substructure for a 2MW turbine

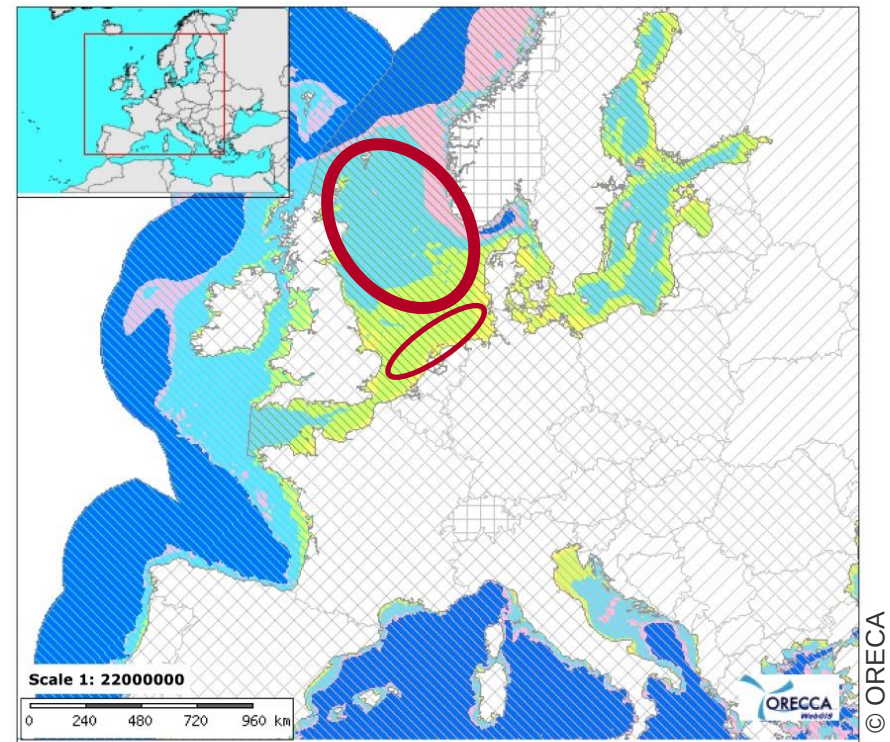


**A cooperation between industry and research institutions**

**Dr.-Ing. Frank Adam**

Offshore Wind R&D Conference 2015, Bremerhaven, 13.10. - 15.10.2015

- Goal of the German Federal Government → 50 % renewable energy by 2050
- Offshore-Windparks → one important role
- LCOE → depending on water depth
- Economical solution → floating foundations



|     |         |
|-----|---------|
| 0   | – 25 m  |
| 25  | – 60 m  |
| 60  | – 200 m |
| 200 | – 500 m |
| ■   | > 500 m |

2014/15

© MitsubishiCorp

2008

© BlueH

2009

© SIEMENS

2013

Spar-Buoy

© WindPower Offshore

2013

Tension Leg Platform (TLP)

© Kesselu News

2011

Barge

© NREL

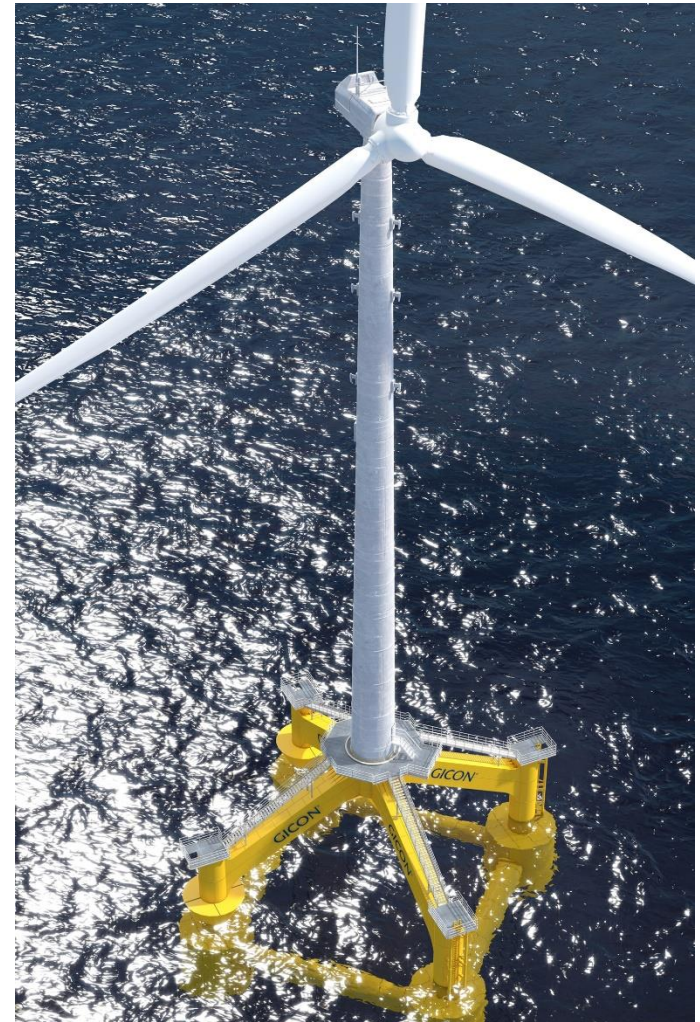
Turbine Concepts

Mooring Line Stabilized

Buoyancy Stabilized "Barge" with mooring



- Economical solution  
→ Mass as low as possible
- Dynamic behavior  
→ Parameter identification
- Boundary conditions  
→ added mass (hydrodynamic mass)
- Scaled tests  
→ Calibration of the calculation model
- Verification of the calculation



TLP for OWT

Calculation-  
model

Verification of  
calculation

Pre-design 6 MW





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Tank tests 2012

Vertical ropes

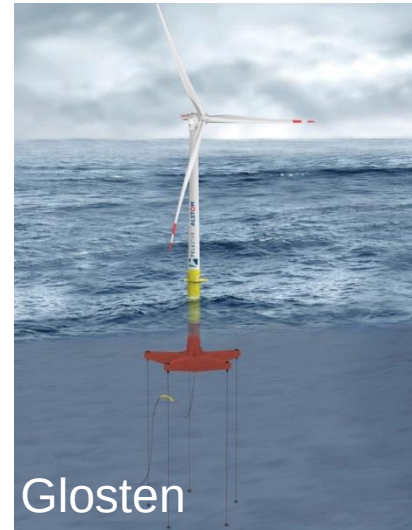
TRL 4



Tank tests 2013

Angled ropes

TRL 3



Tank tests 2013

Vertical ropes

TRL 4



Tank tests 2012-14

Vertical and  
angled ropes

TRL 4-5



|            |          |      |      |     |
|------------|----------|------|------|-----|
| Mass in t  | ca. 2000 | 2214 | 1790 | 742 |
| Width in m | 70       | 68   | 50   | 32  |
| High in m  | 25       | 24   | 39   | 28  |



TLP for OWT

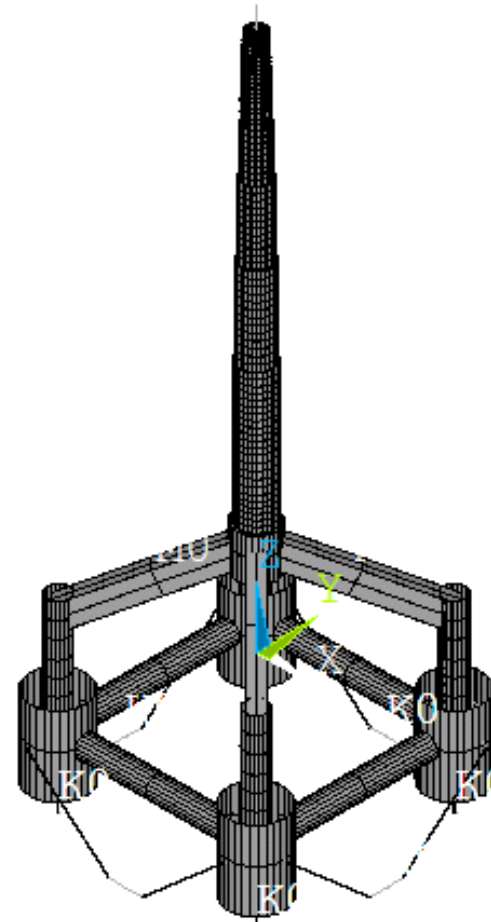
Calculation-  
model

Verification of  
calculation

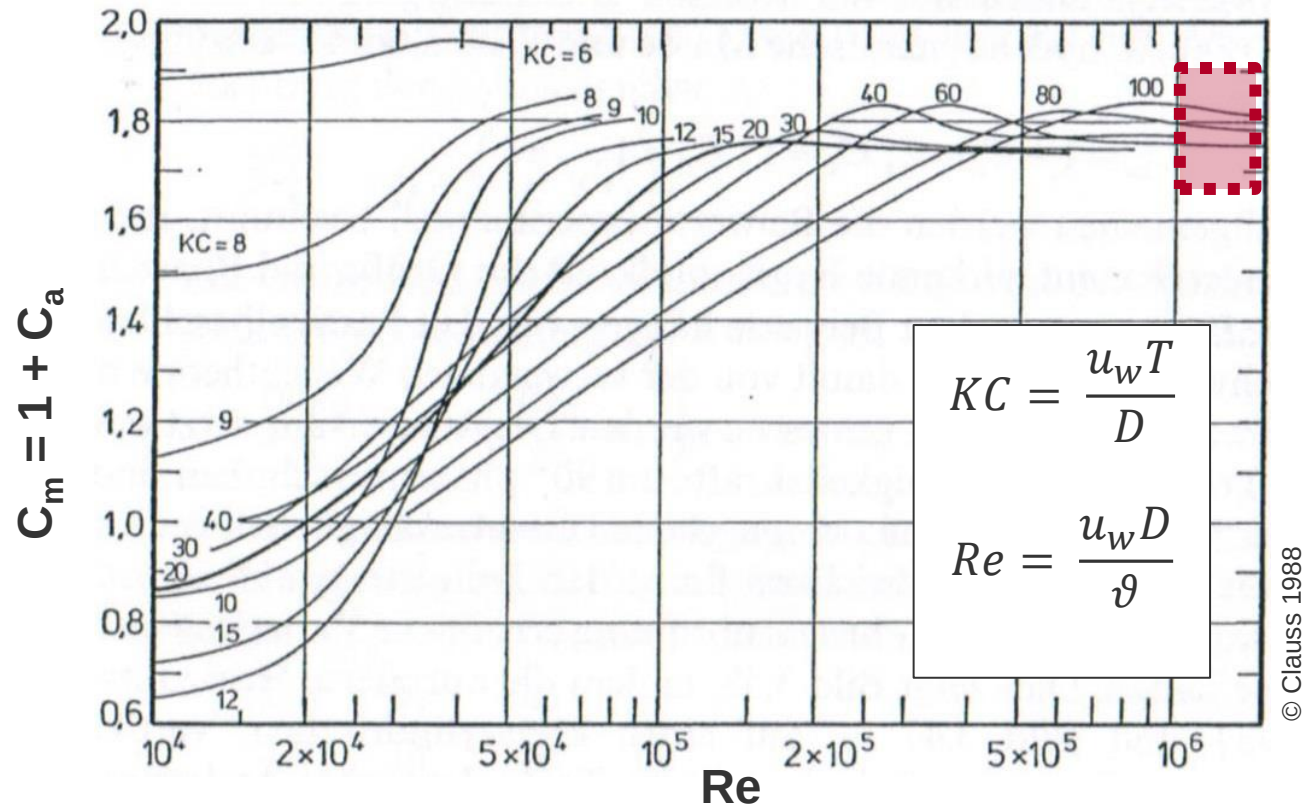
Pre-design 6 MW



- Analysis → FEM
- Tension Leg Platform → Beam elements (1D)
- Damping → Damping elements
- Ropes → Spring elements (only tension)
- MORISON-eq. → Wave loading [Borgman 1954]



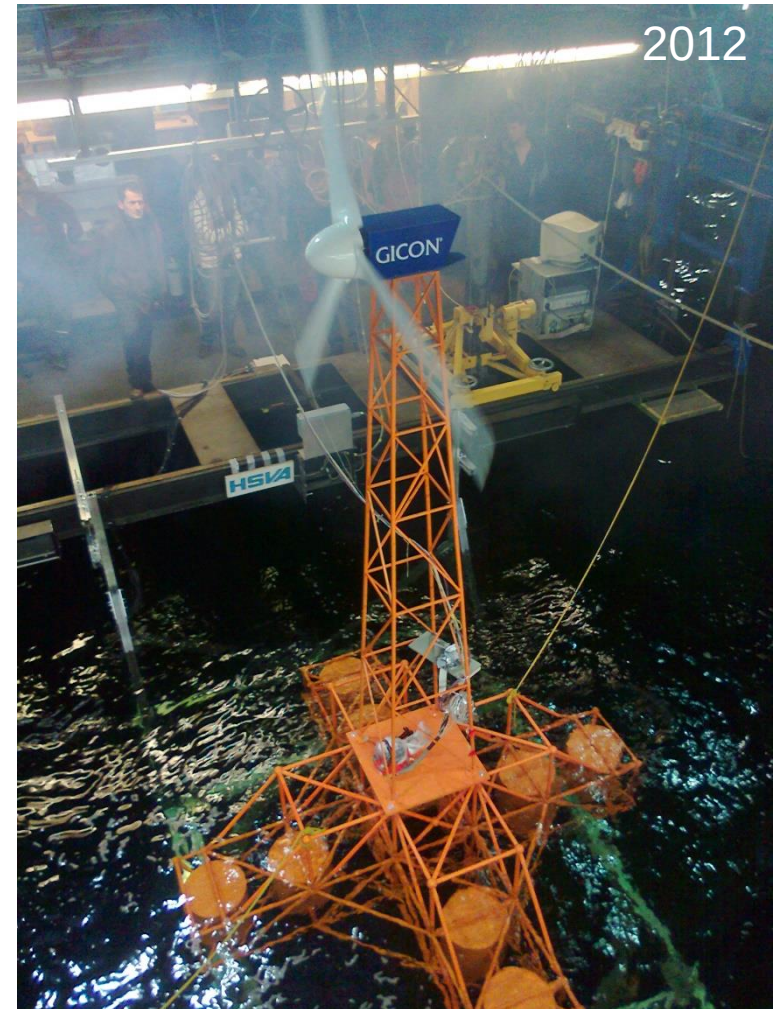
KC ... Keulegan-Carpenter number Re ... Reynolds-number



- For the chosen system  **$Re > 10^6$ ,  $6 \leq KC \leq 190 \rightarrow C_m = 1.8$**



- Question:  $C_m = 1.8$ ?
- Comparison of the measured values with the calculated results (natural frequencies)
- Target value search:  $|f_b - f_m| \rightarrow 0$   
with  $f_b = f_b(C_{a\_Rohr}, C_{a\_AK})$
- Variation of:
  - $0.0 \leq C_{a\_pipe} \leq 0.8$
  - $0.0 \leq C_{a\_BB} \leq 0.8$



TLP for OWT

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Pre-design 6 MW

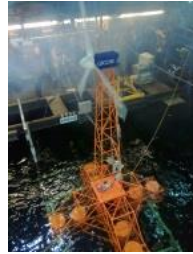






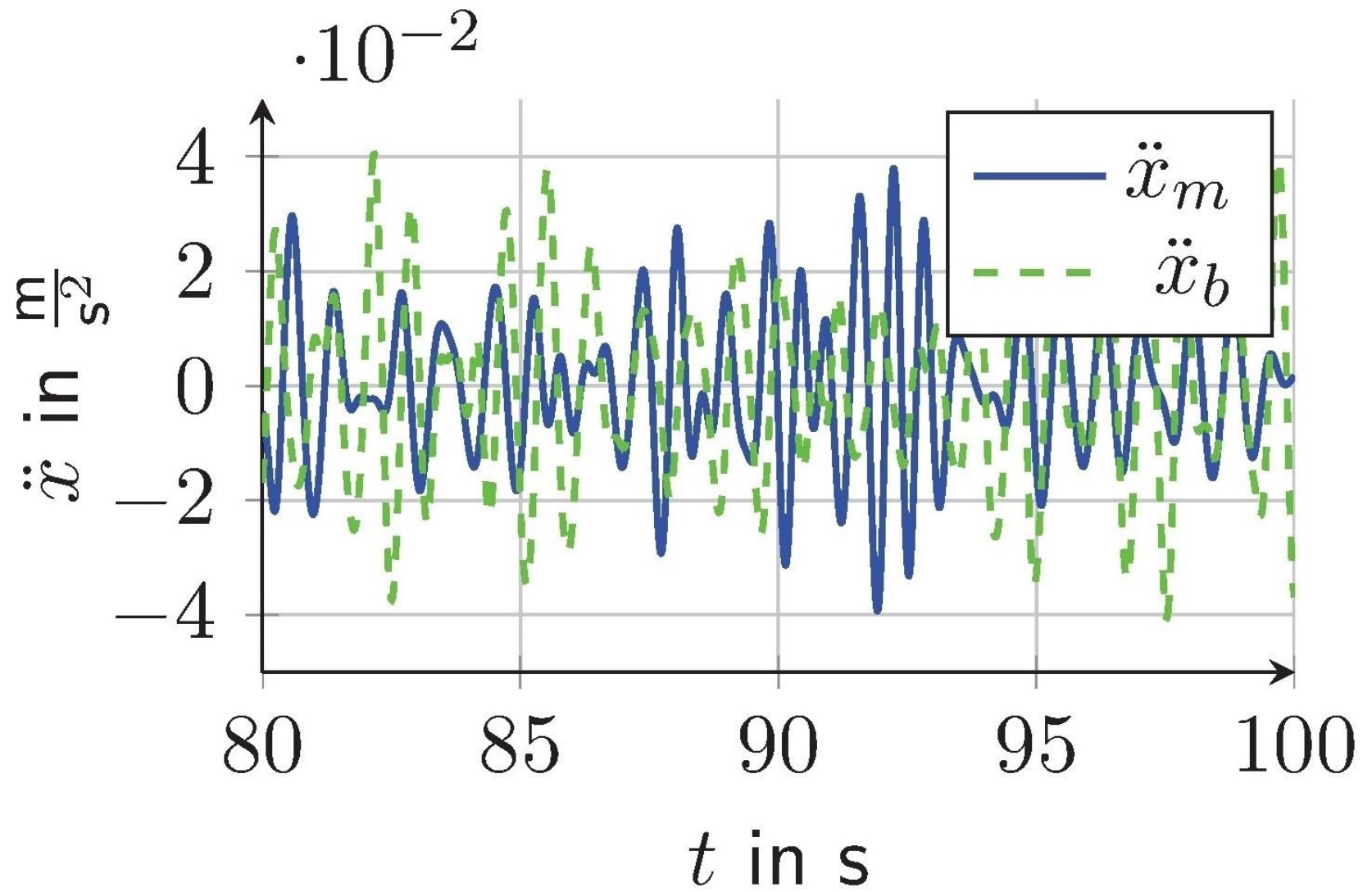
| Facility             | HSVA           | MARIN          | DST                 |
|----------------------|----------------|----------------|---------------------|
| Water depth in m     | 30             | 21             | 21                  |
| Scale                | 1:25           | 1:37           | 1:25                |
| <b>Mooring lines</b> | <b>PE-rope</b> | <b>PE-rope</b> | <b>Flat springs</b> |





|             |       |              |       |              |       |              |
|-------------|-------|--------------|-------|--------------|-------|--------------|
| $x_{trans}$ | 0.270 | <b>0.270</b> | 0.637 | <b>0.625</b> | 0.308 | <b>0.279</b> |
| $y_{trans}$ | 0.254 | <b>0.254</b> | 0.637 | <b>0.625</b> | 0.298 | <b>0.281</b> |
| $z_{trans}$ |       | <b>1.130</b> | 2.111 | <b>1.955</b> |       | <b>1.264</b> |
| $x_{rot}$   | 0.425 | <b>0.425</b> | 1.150 | <b>1.160</b> | 0.608 | <b>0.675</b> |
| $y_{rot}$   | 0.387 | <b>0.387</b> | 1.150 | <b>1.160</b> | 0.667 | <b>0.742</b> |
| $z_{rot}$   | 0.490 | <b>0.490</b> | 1.308 | <b>1.304</b> |       | <b>2.511</b> |

- Agreement for  $C_{a\_BB} = 0.2$  and  $C_{a\_pipe} = 0.6$
- Added mass coefficient → validated for ALL models
- Deduced from the hydrodynamic semi-transparent structure



TLP for OWT

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model

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Pre-design 6 MW





Mass (incl. sec. steel)  $\leq 1200$  t

Floating stability for the sub-structure and anchor incl. wind turbine

Fabrication – 1 ½ sub-TLPs/week

Aim: 80 TLPs/year

Economical solution for water depths  $\geq 30/35$  m – comparable with fixed sub-structures

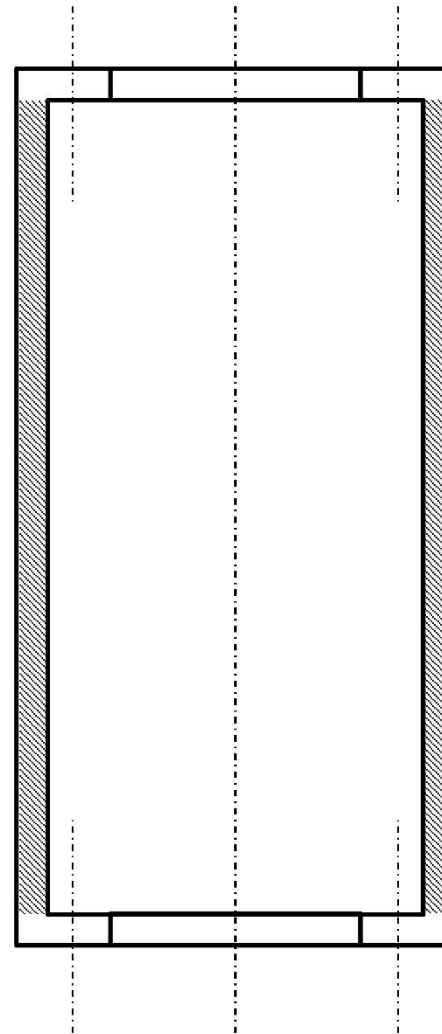
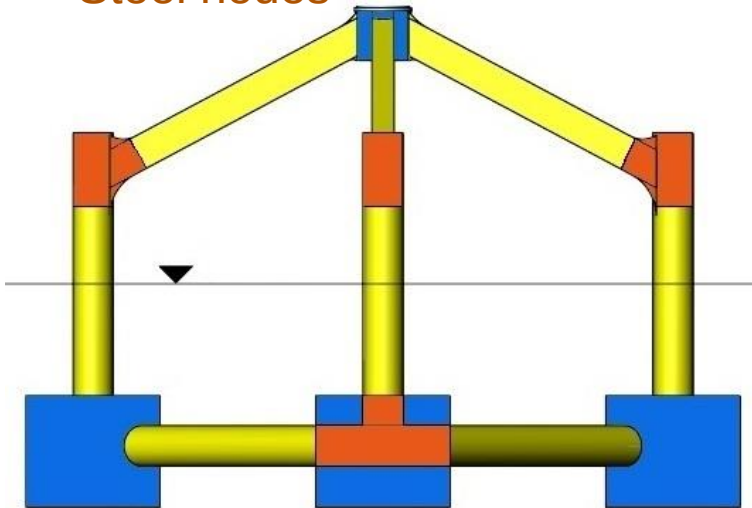


Concrete

Steel-Concrete-Composite

Pipes

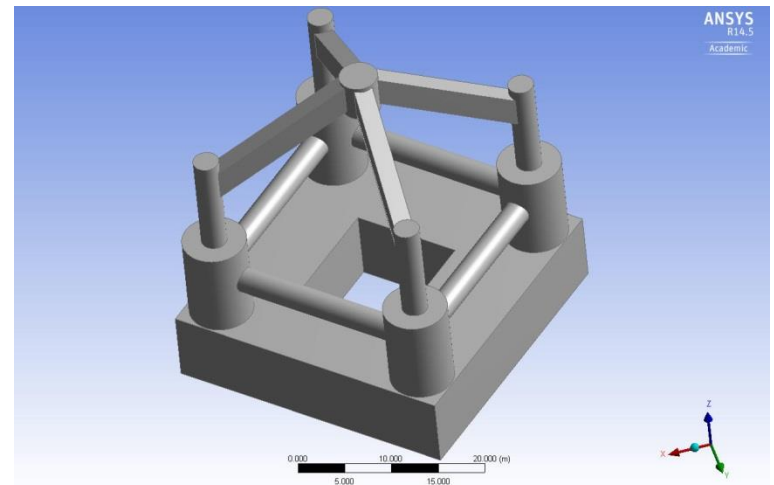
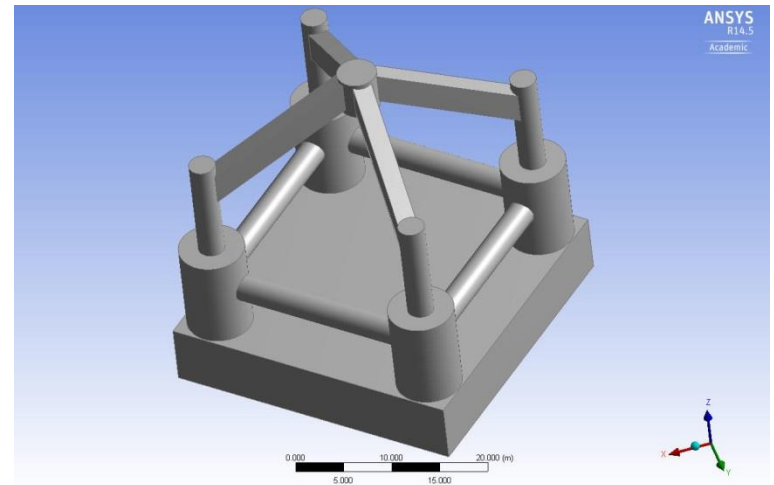
Steel nodes



|                | DeviationMaximum                 |        |        |                  |        |
|----------------|----------------------------------|--------|--------|------------------|--------|
|                | Acceleration (ms <sup>-2</sup> ) |        |        | Rotation(Degree) |        |
| Angle ofAttack | X                                | Y      | Z      | RX               | RY     |
| 180            | -0,616                           | -0,155 | -3,014 | 0,058            | 0,716  |
| 135            | 0,385                            | -0,495 | -2,799 | 0,078            | 0,855  |
| 90             | -0,017                           | -0,661 | -2,716 | 0,164            | -7,970 |
| 45             | -0,384                           | -0,496 | -2,801 | 0,040            | 0,736  |
| 0              | 0,617                            | -0,155 | -3,017 | 0,098            | 4,268  |

|            |       |
|------------|-------|
| Mass       | 5000t |
| WaveFreq   | 0.1Hz |
| WaveHeight | 2m    |

|                | DeviationMaximum                 |        |        |                  |        |
|----------------|----------------------------------|--------|--------|------------------|--------|
|                | Acceleration (ms <sup>-2</sup> ) |        |        | Rotation(Degree) |        |
| Angle ofAttack | X                                | Y      | Z      | RX               | RY     |
| 180            | -0,705                           | -0,101 | -3,281 | 0,104            | 11,971 |
| 135            | -0,411                           | 0,590  | -3,205 | 0,105            | 12,232 |
| 90             | 0,002                            | -0,717 | -3,246 | 0,556            | -0,487 |
| 45             | 0,408                            | 0,591  | -3,209 | 0,043            | 12,426 |
| 0              | 0,705                            | -0,101 | -3,282 | 0,013            | 11,979 |



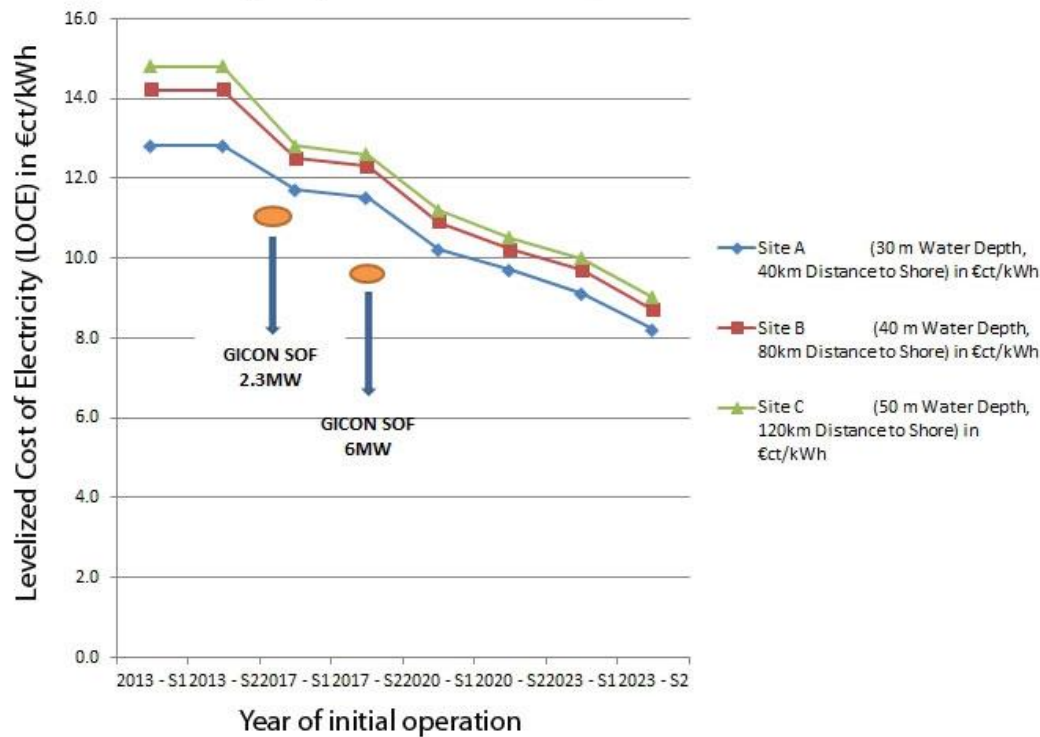


## Conclusion



- First results show the technical feasibility of the 6 MW system
- The system will be an economically viable solution

SOF - Economic Viability highlighted by estimated LCOE  
(independent analysis by ECOVIS based on Prognos Fichtner Scenarios 2013)







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**Prepared by:**

**Dr.- Ing. Frank Adam**

WPC Wind Power Construction GmbH

Carl-Hopp-Straße 4a

18069 Rostock

Phone +49 (0) 174 3236545



